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6 Ocean Tides, Part II.  
A Hydrodynamical Interpolation Model,

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The strictly mathematical ocean tide model developed in Part I of this paper is modified in order to include realistic hydrodynamical barrier effects of narrow ocean ridges and other large bottom irregularities. This modification begins with a hydrodynamical redefinition of the ocean bathymetry at over 3,000 grid points, increasing simultaneously the depth data range to: 10m  $\rightarrow$  7,000m. In a second step a unique hydrodynamical interpolation technique is developed that incorporates into the model over 2,000 empirical tide data collected around the world at continental and island stations. This interpolation is accomplished by a controlled cell-wise adjustment of the bottom friction coefficient and by allowing a monitored in- or out-flow across the mathematical ocean boundary and so, redefining a more physical shoreline. Extensive computer experiments were conducted to study the characteristics of the novel friction laws and hydrodynamical interpolation methods. The computed  $M_2$ -tide data along with all (specially labeled) empirical constants are tabulated in map form for four typical 30° by 50° ocean areas. It is estimated that the tabulated tidal charts permit a prediction of the  $M_2$ -tide elevation of the ocean surface over the geoidal level with an accuracy of better than 5 cm anywhere

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in the open ocean and with somewhat less accuracy near rough shorelines. With the forthcoming construction of the lesser  $S_2$ ,  $N_2$ , and  $K_2$ ;  $K_1$ ,  $O_1$ ,  $P_1$ , and  $Q_1$ ; and  $Mf$ ,  $Mm$ , and  $Ssa$  tidal constituents, the total tide-prediction error can be kept below the 10-cm bound posed by applied researchers of today.

In Part I of this paper (Schwiderski, 1979) a purely hydrodynamical ocean tide model has been developed and tested. This model has been applied to compute a preliminary  $M_2$  ocean tidal chart (Schwiderski, 1976, I). (References listed in Part I are indicated by the added, I, after the year specification.) The results were found encouraging and satisfactory for some applications. However, significant shortcomings still persisted, especially over narrow ocean ridges. The remaining deficiencies were attributed to local distortions and retardations of the tidal waves due to hydrodynamical barrier effects of ocean ridges and other bottom irregularities.

In the following Part II of the paper, an attempt will be made to eliminate the shortcomings of the purely theoretical model by using a hydrodynamically defined bathymetry of the oceans and by incorporating directly empirically known tide data into the discrete tide model described in Part I. The latter modification will be accomplished by a controlled local adjustment of the bottom friction coefficient and by allowing a monitored in- or out-flow across the mathematical ocean boundary, and thus redefining implicitly a more physical shoreline. A detailed discussion of the quality of the new  $M_2$  ocean tidal charts will be given in the sections, "Quality of the Ocean-Tide Model" and "Conclusions."

The complete  $M_2$  ocean tide is published in tabulated map form in Schwiderski (1979c I). Similar charts for the  $S_2$ ,  $N_2$ ,  $K_2$ ,  $O_1$ ,  $P_1$ ,  $Q_1$ ,  $Mf$ ,  $Mm$ , and  $Ssa$  ocean tides (see Part I, Table 1) are under construction and will be published in additional papers. A separate tabulation of the new hydrodynamically defined ocean bathymetry may be found in Schwiderski (1978a I). All tidal and bathymetry data will be available in tape form at the Naval Surface Weapons Center, Dahlgren, Virginia 22448.

### Hydrodynamically Defined Ocean Bathymetry

A reinspection of the bathymetric data revealed clearly that even a  $1^\circ$  by  $1^\circ$  grid scheme falls far short in representing a narrow ocean ridge in a hydrodynamically proper fashion. The defect is particularly compounded when the narrow ridge parallels a deep trench. The reason for this deficiency is obviously the purely hydrostatic character of the averaging principles employed by Smith *et al.* (1966 I) in order to assign a depth value at the center of a mesh cell that is supposed to be representative for the entire cell. For instance, if the area of a mesh cell is (by subjective sight) more than half land, then it is called a "land cell," and the cell is given (for the present purpose) the depth value "zero." In the alternative case, the cell is declared "oceanic," and a depth value is assigned that conserves the estimated actual water mass. Because of those hydrostatic principles, cells were found that contained elongated islands crossing even several cells, but every cell was declared oceanic. Moreover, an oceanic trench portion of the cell with some 7,000-m true depth produced an average depth of more than 3,500 m. Clearly, for ocean current models the entire cell represents an impassable wall, and the depth value should be "zero" instead of 3,500 m.

In order to eliminate the shortcomings of the bathymetric data compiled by Smith *et al.* (1966 I), the depth values were revised by using the following "hydrodynamical" principles:

- (a) Boundary cells at or near continental shorelines consisting of more than half oceanic areas of depths larger than 5 m were designated ocean cells, and the average oceanic depth values were assigned as the "hydrodynamically" averaged depths to the entire cells. The new depth value is preferable to the "hydrostatically" averaged depth, which preserves the actual water mass but ascribes artificially a shallow shelf character to the cell.
- (b) Island cells were declared terrestrial cells with depths zero if either the island areas were larger than half the mesh

areas or the (elongated) island lengths exceeded the mesh diameters.

(c) Island cells that remained oceanic cells were assigned depth values less than the hydrostatically averaged values. In this case and in situations of submerged seamounts or narrow ocean ridges (e.g., Aleutian, Marianas, and Caribbean), the hydrodynamical depths depended on the assessed "barrier" effects of the obstacles: the longer and/or higher the barrier, the lesser the depth. In general, the average "ridge depth" was assigned to the entire cell.

(d) The assigned minimum depth (Part I, Equation 50) was lowered to

$$H_m = \min H(\lambda, \theta) = 20 \text{ m}, \quad (1)$$

which is further lowered to 10 m by the averaging Equations 65 in Part I. (All notations of Part I are used unchanged in the present paper.)

The hydrodynamically justified principles (a) to (c) are, naturally, quite subjective and by no means free of any error. Nevertheless, some computational experiments indicated only very minor effects of isolated depth data changes. More than 3,000 depth values were changed, but only very few of those required additional readjustments in order to keep some limitation on the first and second derivatives of  $H(\lambda, \theta)$ ; i.e., on the relative differences given by Equation 65 in Part I. Furthermore, the hydrodynamical interpolation of empirical tidal data (section, "Hydrodynamical Interpolation of Empirical Tide Data") known at continental and island stations greatly diminishes the need for precise boundary-depth data. The revised depth data bank used in the new tidal computations are published in Schwiderski (1978a I).

### **Empirical Tide Data**

The new tide model incorporates, by a unique hydrodynamical interpolation procedure (next section), empirical tidal data observed

and harmonically analyzed at numerous continental and island stations. These data were taken from publications by the National Ocean Survey (1942), the International Hydrographic Bureau (1966), the British Admiralty (1977 I), and by Pekeris and Accad (1969 I), Zahel (1970 I, 1973 I), Cartwright (1971), and Luther and Wunsch (1975 I). Unfortunately, the most recent publication by the British Admiralty lists harmonic constants only for the four major tide components  $M_2$ ,  $S_2$ ,  $K_1$ , and  $O_1$  and excludes the European waters completely.

The voluminous data banks had to be screened in order to eliminate observations that are meaningless or unreliable for the present ocean-tide investigations. For example, tidal constants were excluded that were listed for stations deep inside estuaries or narrow bays (e.g., Hudson River, Bay of Fundy), at the mouths of large rivers (e.g., Amazon), between sheltering islands (e.g., Alexander Archipelago, Solomon Islands), and inside sheltering reefs (e.g., Great Barrier Reef).

About 2,500 stations were selected for further examination of their data concerning locally restricted distortions. For instance, some data taken over short distances along a coastline displayed rather drastically alternating times of high water, which are obviously meaningless for oceanic tidal studies. At many stations, different tables give different tidal constants. Some of those discrepancies at island stations are shown for the  $M_2$ -tide in Table 1. Similarly, for some mesh cells, several different station data were available, and only one representative average had to be chosen. This situation is illustrated in Table 2 for the  $M_2$ -tide around Bermuda. Many of those differences can probably be explained as simple errors in printing or computing. For instance, the phase difference of about 1 hr at Port Galets on La Reunion Island (Table 1) seems to be due to some error in observing the correct reference time, which varies from listing to listing. Most differences, such as those shown for Bermuda stations in Table 2, are definitely true local variations. In this connection, the important tidal measurements by Gallagher *et al.* (1971) at Fanning Atoll in the central Pacific may be men-

**Table 1**  
**Empirical M<sub>2</sub>-tide differences.**

Station Latitude, Longitude		B.A.T.(77) <sup>a</sup>		N.O.S.(42) <sup>b</sup>		Others Initialed	
		$\xi(m)$	$\alpha(^{\circ})$	$\xi(m)$	$\alpha(^{\circ})$	$\xi(m)$	$\alpha(^{\circ})$
Tenerife, Canary Island	(A)	0.67				0.69	Z <sup>c</sup>
28°29'N 16°14'W			18				30
Port Praia, Cape Verde I.	(A)	0.42				0.43	Z <sup>c</sup>
14°55'N 23°31'W			244				220
Ascension Island	(A)	0.33				0.51	P,Z
7°55'S 14°25'W			177				174
St. Helena Island	(A)	0.32				0.34	P,Z
15°55'S 5°42'W			81				87
Tristan da Cunha Island	(A)	0.23				0.34	P,Z
37°02'S 12°18'W			12				354
Agalega Island	(I)	0.29				0.29	Z
10°28'S 56°40'E			350				290
Port Galets, La Reunion I.	(I)	0.16		0.14		0.14	Z
20°55'S 55°17'E			302		328		328
Mawson, Antarctica	(I)	0.04				0.04	Z
67°36'S 62°53'E			232				155
Wilkes Station, Antarctica	(I)	0.28				0.38	Z
66°15'S 110°31'E			162				140
Welles Harbor, Midway I.	(P)	0.11				0.11	P,Z
28°12'N 117°22'W			82				91
Eniwetok Atoll, Marshall I.	(P)	0.36		0.36			
11°21'N 162°21'E			127		137		
Les Wallis, Fiji Island	(P)	0.53		0.52			
13°22'S 176°11'W			178		154		
Suva Harbor, Viti Levu,							
Fiji Island	(P)	0.56		0.50			
18°09'S 178°28'E			195		212		

<sup>a</sup> B.A.T.(77) = British Admiralty Tables (1977 I).

<sup>b</sup>  $\xi$  = tidal amplitude.

<sup>c</sup>  $\alpha$  = tidal phase relative to Greenwich.

<sup>d</sup> N.O.S. (42) = National Ocean Survey (1942).

<sup>e</sup> Z = Zahel (1970 I).

<sup>f</sup> P = Peteris and Accad (1969 I).

tioned. Tides outside and inside the small atoll's lagoon differed by about 50% (20 cm) in amplitude and by a phase lag of about 50° (1 hr, 40 min.).

In general, the most recent listings in the British Admiralty Tide

Tables (1977 I) were chosen over older tabulations as the most reliable. The selection of the data was further aided by earlier and subsequent tidal computations. Altogether, some 1,700  $M_2$ -tide data were selected and assigned to the centers of their respective mesh cells. Using linear interpolation and tidal computations, the total number of prescribed tide data used in the  $M_2$ -tide construction was increased to more than 2,000. Essentially all continental boundary cells carry empirically supported tide data. The empirical coverage is only marginal at arctic and antarctic shorelines. Most empirical tide data known at island stations are also included in the tide model.

Naturally, it must be remembered that the selection of representative, empirical tidal data (compare depth data, section before "Hydrodynamically Defined Ocean Bathymetry") is not at all free of subjective judgment and may be somewhat erratic. Obviously, only future additional tidal measurements can improve this model

Table 2  
Bermuda  $M_2$ -tide observations.

Station Latitude, Longitude	$\epsilon$ (cm)	$\phi$ (°)	Reference
St. George's Island 32.56N, 64.70W	36	359	British Admiralty (1977 I)
St. David's Island 32.37N, 64.65W	34	355	British Admiralty (1977 I)
Great Sound 32.32N, 64.63W	34	6	British Admiralty (1977 I)
St. George's Island 32.37N, 64.70W	35	0	National Ocean Survey (1942)
St. George's Island 32.40N, 64.70W	37	0	Pekeris and Accad (1969 I)
St. George's Island 32.37N, 64.70W	36	359	Zahel (1970 I)
St. George's Island 32.40N, 64.70W	36	358	Zettler et al. (1975)
Deep Sea (GOBI IV) 32.28N, 64.60W	36	11	J. T. Kuo Letter (1977)

$\epsilon$  = tidal amplitude.

$\phi$  = tidal phase relative to Greenwich.

in this respect. Nevertheless, according to the instruction notes accompanying the British Admiralty Tide Tables (1977 I), it can probably be assumed that almost all important tide data selected carry an accuracy that is at least as high as the desired 10 cm. In any case, computational experiments showed that isolated reasonable variations of the boundary-tide data do not affect significantly the adjacent oceanic tides. It was also found insignificant to the overall quality of the tide model whether the empirical data were assigned to the centers or to the shore boundaries of the respective cells.

Attempts were made to incorporate also recent deep-sea tidal measurements into the present model. Since the hydrodynamical interpolation of empirical data is essentially based on bottom and boundary irregularities (see next section (a)–(d)), no physically valid justification was found to include distant offshore deep-sea measurements into the model. However, some deep-sea measurements near rough shore and bottom areas were included. Fortunately, without exception, all excluded offshore deep-sea measurements known to the author agree very well with the computed  $M_2$ -tide data (see Table 3).

**Table 3a**  
**Deep-sea  $M_2$ -tide data for the Gulf of Mexico and Caribbean Sea.**

Station Latitude, Longitude	Observed		Model		Error	
	$\xi$ (cm)	$\theta$ (°)	$\xi$ (cm)	$\theta$ (°)	$\Delta\xi$ (cm)	$\Delta\theta$ (°)
W. Florida Shelf St. 26.71N, 84.25W	7	97	7	92	0	–5
Deep Gulf St. 24.77N, 89.65W	1.3	226	1.6	225	+0.3	–1
Misteriosa Bank 18.88N, 83.81W	8	84	9	89	+1	+5
Rosalind Bank 16.61N, 80.34W	7	107	8	102	+1	–5
East Carib. St. (6-month) 16.54N, 84.88W	0.5	156	1.6	151	+1	–5
East Carib. St. (1-month) 16.52N, 84.91W	0.6	153	1.5	148	0.9	–5

$\xi$  = tidal amplitude.

$\theta$  = tidal phase relative to Greenwich.



**Table 3b**  
**Deep-sea  $M_2$ -tide data for the Pacific and Atlantic oceans.**

Station Latitude, Longitude	Observed		Model		Error	
	$\xi^a(\text{cm})$	$\delta^b(^{\circ})$	$\xi(\text{cm})$	$\delta(^{\circ})$	$\Delta\xi(\text{cm})$	$\Delta\delta(^{\circ})$
Pacific St. 1 (Middleton)	110		included			
58.76N, 145.71W		284				
Pacific St. 3 (Tofino)	99		included			
48.97N, 127.29W		239				
Pacific St. (San Francisco)	54		included			
38.16N, 124.91W		227				
Pacific St. (Josie II)	27		27		0	
34.00N, 144.99W		267		273		+6
Pacific St. (Flicki)	43		included			
32.24N, 120.86W		149				
Pacific St. (Josie I)	43		included			
31.03N, 119.80W		142				
Pacific St. (Kathy)	29		27		-2	
27.75N, 124.37W		128		130		+2
Pacific St. (Filloux)	19		18		-1	
24.78N, 129.02W		107		105		-2
Atlantic St. 1 (N.Y. Bight)	44		included			
39.32N, 64.36W		350				
Atlantic St. (N.C. St. 1)	48		46		-2	
32.69N, 75.62W		356		358		+2
Atlantic St. (Savannah B)	88		included			
31.95N, 80.68W		15				
Atlantic St. (Scope)	45		46		+2	
30.43N, 76.42W		358		3		+5
Atlantic St. (AOML 1)	34		35		+1	
28.14N, 69.75W		1		6		+5
Atlantic St. (AOML 3)	34		34		0	
28.24N, 67.54W		359		4		+5
Atlantic St. (MERT)	34		34		0	
27.99N, 69.67W		360		6		+6
Atlantic St. (REIKO)	35		34		-1	
27.97N, 69.67W		1		6		+5
Atlantic St. (EDIE-May)	32		32		0	
26.48N, 69.33W		3		7		+4
Atlantic St. (EDIE-March)	31		32		+1	
26.45N, 69.32W		1		7		+6

<sup>a</sup>  $\xi$  = tidal amplitude.

<sup>b</sup>  $\delta$  = tidal phase relative to Greenwich.

Of course, the continuity gap (Equation 4) can be attributed to the following major causes which are physically plausible:

- (a) The bottom-friction coefficient,  $b$  (in  $A^4$  and  $B^4$  of Equations 62 in Part I), which is most effective in boundary cells, depends on local shore features such as true cell size and bottom slope and roughness.
- (b) The boundary cells are idealized by definition of strictly mathematical boundaries (see Figure 1).
- (c) The depth data of boundary cells are subjectively defined and, hence, faulty (section, "Hydrodynamically Defined Ocean Bathymetry").
- (d) The empirical tidal constants in Equation 3 are also faulty to some degree because of inaccurate measurements, harmonic analyses, and subjective selections and assignments to the centers of the boundary cells (preceding section).
- (e) The discrete ocean-tide model is certainly not an exact description of the true oceanic tide; e.g., at boundaries, non-linear inertial terms assume significance.

Obviously, the last two (hopefully minor) faults can be reduced only through continued future observations and modeling. However, the first two faults, (a) and (b), can be weakened by "hydrodynamically interpolating" the empirical tidal elevations (Equation 3) into the tidal model and narrowing the continuity gap (Equation 4) to an acceptable level as follows:

- (A) Adjusting the velocity field by a locally controlled implicit variation of the bottom-friction coefficient,  $b$ , in Equations 62 Part I.
- (B) Lifting the strict condition of no-flow across the mathematical ocean boundary and allowing for a monitored in- or out-flow by implicitly defining a more physical ocean boundary (Figure 1).

As was pointed out in Part I, section, "The Discrete Ocean-Tide Equations (DOTEs)," due to the choice of the finite-difference

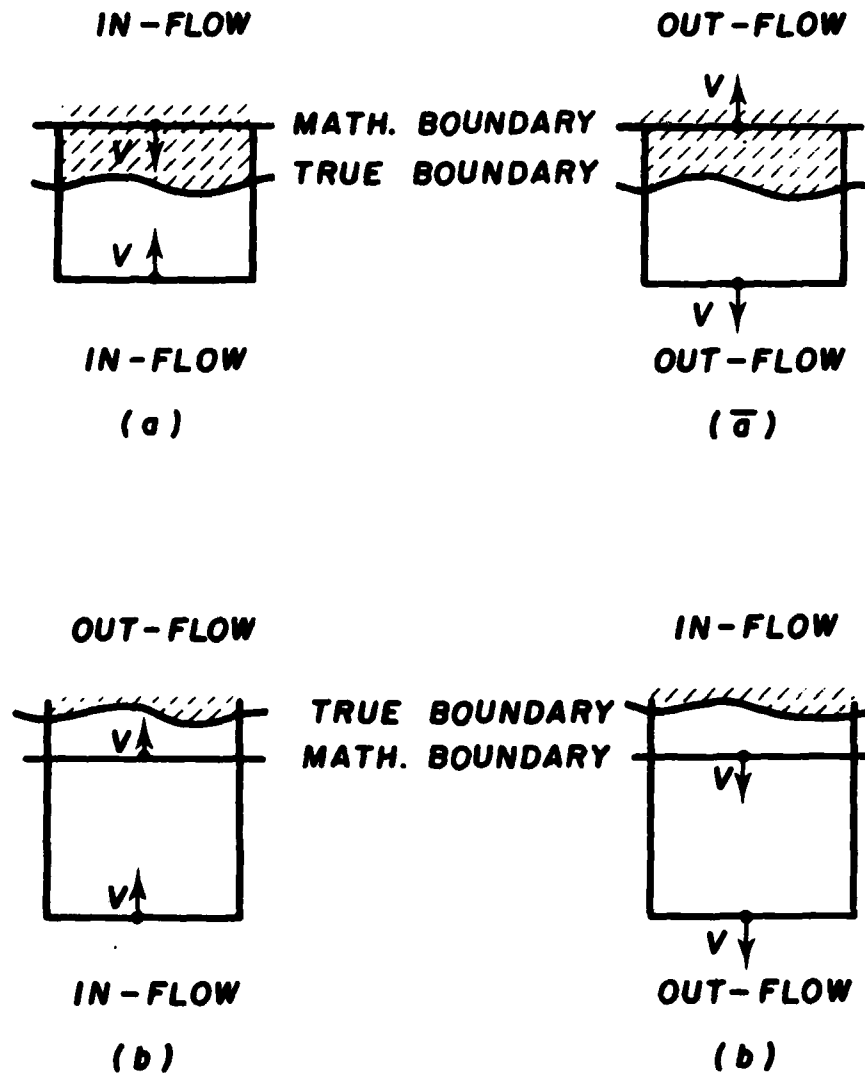


Figure 1. Boundary cell in- and out-flow illustration: (a) and (a-bar), also (b) and (b-bar) are half-periods apart. (Shaded region is land area.)

parameter  $\kappa = 1$ , the bottom friction coefficient,  $b$ , in  $A^4$  and  $B^4$  of the momentum equations (Part I, Equations 60) can be considered implicitly varied in the mesh cell  $S_{m,n}$  by directly replacing the velocity components in Equation 2 as follows:

$$\begin{aligned}
 U_{m,n}^{j+1} &\rightarrow U_{m,n}^{j+1} + |U_{m,n}^{j+1}| (w u_1 + w \bar{u}_1), \\
 U_{m+\mu,n}^{j+1} &\rightarrow U_{m+\mu,n}^{j+1} + |U_{m+\mu,n}^{j+1}| (w u_2 + w \bar{u}_2), \\
 V_{m,n}^{j+1} &\rightarrow V_{m,n}^{j+1} + |V_{m,n}^{j+1}| (w v_1 + w \bar{v}_1),
 \end{aligned} \tag{5}$$

and

$$V_{m,n-1}^{j+1} \rightarrow V_{m,n-1}^{j+1} + |V_{m,n-1}^{j+1}| (w v_2 + w \bar{v}_2),$$

provided  $\xi_{m,n} \neq 0$ ; i.e., provided an empirical tidal amplitude is available for the considered mesh cell. In Equation 5, the consistency and scale parameters  $(u, \bar{u})$  and  $(v, \bar{v})$  are defined by

$$\begin{cases} u_1 = 1, \bar{u}_1 = 0 & \text{for } \Delta \zeta_{m,n}^{j+1} \cdot U_{m,n}^{j+1} < 0, \\ u_1 = 0, \bar{u}_1 = A_{m,n}^4 & \text{otherwise, but} \\ u_1 = 0, \bar{u}_1 = 0 & \text{if } \tilde{\xi}_{m-\mu,n} \neq 0; \end{cases} \tag{6a}$$

$$\begin{cases} u_2 = 1, \bar{u}_2 = 0 & \text{for } \Delta \zeta_{m,n}^{j+1} \cdot U_{m-\mu,n}^{j+1} > 0, \\ u_2 = 0, \bar{u}_2 = A_{m+\mu,n}^4 & \text{otherwise;} \end{cases} \tag{6b}$$

$$\begin{cases} v_1 = 1, \bar{v}_1 = 0 & \text{for } \Delta \zeta_{m,n}^{j+1} \cdot V_{m,n}^{j+1} < 0, \\ v_1 = 0, \bar{v}_1 = B_{m,n}^4 & \text{otherwise;} \end{cases} \tag{6c}$$

and

$$\begin{cases} v_2 = 1, \bar{v}_2 = 0 & \text{for } \Delta \zeta_{m,n}^{j+1} \cdot V_{m,n-1}^{j+1} > 0, \\ v_2 = 0, \bar{v}_2 = B_{m,n-1}^4 & \text{otherwise, but} \\ v_2 = 0, \bar{v}_2 = 0 & \text{if } \xi_{m,n-1} \neq 0. \end{cases} \tag{6d}$$

The continuity gap (Equation 4) will be narrowed when the "control parameters"  $w$  and  $\bar{w}$  are determined successively by:

$$w = \begin{cases} \Delta \zeta_{m,n}^{j+1} / \zeta & \text{for } \zeta \neq 0, \\ 0 & \text{for } \zeta = 0 \end{cases} \tag{7a}$$

with the first "control limit"

$$|w| \leq k_1 \quad (7b)$$

and

$$w = \begin{cases} [\Delta \zeta_{m,n}^{j+1} - w\zeta] / \bar{\zeta} & \text{for } \bar{\zeta} \neq 0, \\ 0 & \text{for } \bar{\zeta} = 0 \end{cases} \quad (8a)$$

with the second control limit

$$|w| \leq k_1 \quad (8b)$$

where (see Equation 3)

$$\begin{aligned} \zeta &= C_n^1 [u_1 |U_{m,n}^{j+1}| + u_2 |U_{m+\mu,n}^{j+1}|] + v_1 C_n^2 |V_{m,n}^{j+1}| + v_2 C_n^3 |V_{m,n-1}^{j+1}| \\ \text{and} \\ \bar{\zeta} &= C_n^1 [\bar{u}_1 |U_{m,n}^{j+1}| + \bar{u}_2 |U_{m+\mu,n}^{j+1}|] + \bar{v}_1 C_n^2 |V_{m,n}^{j+1}| + \bar{v}_2 C_n^3 |V_{m,n-1}^{j+1}| \end{aligned} \quad (9)$$

It is important to note that  $u_i \cdot \bar{u}_i = 0$  and  $v_i \cdot \bar{v}_i = 0$  for  $i = 1, 2$ . Accordingly, both control limits,  $k_1$  and  $k_2$ , which are at one's disposal, regulate the allowed decrease or, respectively, increase of the velocity components in Equations 5; i.e., the implicitly permitted corresponding increase or decrease of the local bottom-friction coefficients. Since the integration sweeps across the ocean from  $m = \mu$  to 360 and  $n = 4$  to 168, the special choice of  $u_1 = \bar{u}_1 = 0$  and  $v_2 = \bar{v}_2 = 0$  in Equations 6a and 6d excludes possible double adjustments of the velocity components. Also, if  $u_1 \neq \bar{u}_1$  and/or  $v_2 \neq \bar{v}_2$ , backward adjustments of the tidal elevations via the corresponding Equation 2 must be made. This requires the replacements

$$\begin{aligned} \zeta_{m-\mu,n}^{j+1} &\rightarrow \zeta_{m-\mu,n}^{j+1} - C_n^1 |U_{m,n}^{j+1}| (w u_1 + \bar{w} \bar{u}_1) \\ \text{and} \\ \zeta_{m,n-1}^{j+1} &\rightarrow \zeta_{m,n-1}^{j+1} - C_n^2 |V_{m,n-1}^{j+1}| (w v_2 + \bar{w} \bar{v}_2). \end{aligned} \quad (10)$$

Analogous substitutions in the forward directions of  $m$  and  $n$  follow automatically in the integration process.

The velocity replacements in Equations 5 may be illustrated by the example

$$\left. \begin{aligned} U_{m,n}^{j+1} &> 0, U_{m+\mu,n}^{j+1} > 0, V_{m,n}^{j+1} > 0, V_{m,n-1}^{j+1} \geq 0, \\ \Delta \zeta_{m,n}^{j+1} &> \tilde{\xi}_{m-\mu,n} = 0, \tilde{\xi}_{m,n-1} \neq 0. \end{aligned} \right\} \quad (11)$$

One finds  $w > 0$ ,  $\bar{w} \geq 0$ , and

$$\left. \begin{aligned} U_{m,n}^{j+1} &\rightarrow U_{m,n}^{j+1}(1 + \bar{w}A^4), \\ U_{m+\mu,n}^{j+1} &\rightarrow U_{m+\mu,n}^{j+1}(1 - w), \\ V_{m,n}^{j+1} &\rightarrow V_{m,n}^{j+1}(1 + \bar{w}B^4), \end{aligned} \right\} \quad (12)$$

and

$$\zeta_{m-\mu,n}^{j+1} \rightarrow \zeta_{m-\mu,n}^{j+1} - C_n^1 U_{m,n}^{j+1} \bar{w} A^4$$

At this point, it must be mentioned that attempts were explored to lift the control limits prescribed by  $k_1$  and  $k_2$  in Equations 7b and 8b in an effort to close the continuity gap completely. However, since the bottom-friction coefficient,  $b$ , is rather small the control limits,  $k_1$  and  $k_2$ , had to be kept small to achieve best results. Computations conducted with large control limits  $k_1$  (excessive bottom friction) seemed to close the continuity gap, but the tidal and velocity fields in the open oceans assumed unrealistically small values. Large control limits  $k_2$  (insufficient bottom friction) produced strong instabilities as anticipated from the analysis in the section, "Stability Analysis," of Part I. To safely check the possible instability, the second control parameter  $\bar{w}$  (Equations 5, 6, and 12) was defined in units of  $\bar{u} = A^4$  and  $\bar{v} = B^4$ , in contrast to  $u = 1$  and  $v = 1$ , used for the first control parameter  $w$ .

After some trial-and-error computations, the following control limits were chosen for the  $m_2$ -tide model:

$$k_1 = 0.03, k_2 = 0.06. \quad (13)$$

These moderate values reflect the well-known fact that the magnitude of bottom friction has a strong effect on the motions considered. Indeed, with some minor improvements of the tidal field, significant improvements of the continuity gap, velocity field, and convergence of the integration were achieved. This procedure was applied to all oceanic cells with known empirical tide data (Equation 3), provided these cells bordered terrestrial cells or contained small islands or other bottom irregularities. No meaningful reason was seen to apply the same bottom-friction adjustment procedure to distant offshore oceanic cells with available deep-sea tide measurements.

In order to implement the second step (B) of the hydrodynamical interpolation procedure, the following velocity replacements in oceanic mesh cells bordering terrestrial cells were defined:

$$\left. \begin{aligned} U_{m,n}^{j+1} &\rightarrow \tilde{w}\tilde{u}_1 U_{m+\mu,n}^{j+1}, \\ U_{m+\mu,n}^{j+1} &\rightarrow \tilde{w}\tilde{u}_2 U_{m,n}^{j+1}, \\ V_{m,n}^{j+1} &\rightarrow \tilde{w}\tilde{v}_1 V_{m,n-1}^{j+1} \end{aligned} \right\} \quad (14)$$

and

$$V_{m,n-1}^{j+1} \rightarrow wv_2 V_{m,n}^{j+1},$$

provided  $\tilde{\xi} \neq 0$  in Equation 3. The parameters  $(\tilde{u}\tilde{v})$  are mutually consistent by definition:

$$\left. \begin{aligned} \tilde{u}_1 &= 1 \text{ if } U_{m,n}^{j+1} = 0, \text{ otherwise } \tilde{u}_1 = 0, \\ \tilde{u}_2 &= 1 \text{ if } U_{m+\mu,n}^{j+1} = 0, \text{ otherwise } \tilde{u}_2 = 0, \\ \tilde{v}_1 &= 1 \text{ if } V_{m,n}^{j+1} = 0, \text{ otherwise } \tilde{v}_1 = 0, \end{aligned} \right\} \quad (15)$$

and

$$\tilde{v}_2 = 1 \text{ if } V_{m,n-1}^{j+1} = 0, \text{ otherwise } \tilde{v}_2 = 0.$$

The remaining continuity gap will be further narrowed when the control parameter  $\tilde{w}$  is determined to be in agreement with Equations 2, 4, 7, 8, and 9 by

$$\tilde{w} = \begin{cases} [\Delta \zeta_{m,n}^{t+1} - w\zeta - \bar{w}\bar{\zeta}] / \tilde{\zeta} & \text{for } \tilde{\zeta} \neq 0 \\ 0 & \text{for } \tilde{\zeta} = 0 \end{cases} \quad (16a)$$

with the third control limit

$$|\tilde{w}| \leq k_3, \quad (16b)$$

where

$$\tilde{\zeta} = C_n^1 [\tilde{u}_1 U_{m,n}^{t+1} - \tilde{u}_2 U_{m,n}^{t+1}] + \tilde{v}_1 C_n^2 V_{m,n-1}^{t+1} - \tilde{v}_2 C_n^2 V_{m,n}^{t+1}. \quad (17)$$

Obviously, the substitutions (Equations 14) specify consistent in- or out-flows across the mathematical boundaries of oceanic coastal cells, as illustrated in Figure 1, without explicitly fixing the physical boundary line. Again, no complete removal of the continuity gap was possible. The most satisfactory results for the M<sub>2</sub>-tide were achieved by setting the third control limit (Equation 16b) at

$$k_3 = 0.5. \quad (18)$$

While the improvement of the tidal field was again moderate, the remaining continuity gaps and nearshore velocity distortions assumed uniformly satisfactory levels. The remaining small shortcomings of the model can easily be attributed to the boundary inaccuracies (c), (d), and (e) listed above, but for which no simple remedies were found.

It may be emphasized that the rather significant change in the nearshore velocity field permitted by the in- and out-flow specifications (Equations 14) affected the tidal field only in a minor fashion. This important phenomenon is in agreement with the well-known fact that the pressure distribution in a fluid motion is very insensitive to large but local velocity variations. For instance, it is perhaps the most important postulate in Prandtl's boundary-layer theory (see, e.g., Schlichting, 1968 I), and it is the basis of the hydro-



static-pressure assumption invoked here and in the section, "The Continuous Ocean-Tide Equations (COTEs)," of Part I for the present tidal model.

The hydrodynamical interpolation technique considerably accelerated the convergence of the integration procedure toward the steady state amplitudes and phases. In fact, the computation of the new  $M_2$ -tide model (sections, "Quality of the Ocean-Tide Model" and "Conclusions") was terminated when the amplitudes and phases over all open ocean areas differed by less than 1 cm and  $1^\circ$ , respectively. Obviously, this improved convergence feature goes significantly beyond the same property described in Part I, section, "Lateral-Boundary, Initial and Final Data," for the purely mathematical model.

### Quality of the Ocean-Tide Model

Since the present tide model incorporates essentially all known empirical data by hydrodynamical interpolation (preceding section), no direct comparison of observed and computed data is feasible. Nevertheless, a comprehensive appraisal of the reality of the present tide model is possible by inspecting the quality of hydrodynamical interpolation; i.e., by evaluating the "smoothness" with which the computed tide "accepts or rejects" the empirical tidal data. In fact, the smoothness characteristics of the novel hydrodynamical interpolation technique are distinctly different from those of other direct interpolation procedures using power or trigonometric polynomials. In the latter case, smoothness of the interpolation can be carried up to any desired degree by simple design. The adjustment of hydrodynamical parameters (preceding section) in the former method does not imply any smoothness of the interpolation, unless both the empirical input data and the hydrodynamical tide model are compatible with each other.

As is well known, local tidal distortions, caused by an isolated roughness (seamount or small island) in the bottom relief, affect the surrounding ocean tide very little. The major level of ocean tides is shaped by continental shorelines and large (in area and/or length) islands and ridges. In contrast to ordinary polynomial in-

terpolations, an important feature of the new hydrodynamical interpolation method is that it preserves those significant properties of ocean tidal currents without any essential alterations.

Extensive computer experiments were conducted to test the important smoothness characteristics of the hydrodynamical interpolation procedure. Faulty input data were deliberately inserted and quickly recognized as rejected by the computed surrounding tide. Indeed, the first computations, which included empirical tidal data, revealed immediately several input errors in the data. Vice versa, smoothly accepted empirical tidal data were randomly deleted to test their backlash reaction on the computed tide. As anticipated, no significant modifications were detected. Consequently, the hydrodynamical interpolation technique permits a check of the reality of both the tide model and the empirical tidal input data. If an input value is rejected by the computed tide, then one or the other or both are defective. Fortunately, only very few discrepancies between the different sources of observed  $M_2$ -tide data (see section, "Empirical Tide Data") have been discovered that way.

The new discrete tide-model has been applied to compute the global  $M_2$  ocean tide. A complete discussion and tabulation of all amplitudes and phases is presented in Schwiderski (1979c I). In order to display the quality of the tidal model, the computed amplitudes (in cm) and phases (in degrees) along with their adjacent empirical values have been tabulated in "30° by 50° map form" for four typical ocean areas (Tables 4-7). All empirically supported input data along continental shores and at island stations are underlined in the tables. All nearshore deep-sea measurements included in the model are labeled by subbrackets. As was explained in the preceding section, all distant offshore deep-sea measurements are not included in the tide model. However, their approximate locations are marked by wavy underlines, and their corresponding observed data are listed in Table 3. Land points are left blank.

In the evaluation of the tidal accuracy, one must remember that the ocean tide at any fixed location is determined by two harmonic constants. If  $(\xi, \delta)$  and  $(\xi', \delta')$  denote the respective local amplitudes and phases of the "true" and "computed" tides

$$\zeta_0 = \xi_0 \cos(\sigma t - \delta_0), \zeta = \xi \cos(\sigma t - \delta), \quad (19)$$

then their time-dependent error is

$$\tilde{\zeta} = \zeta_0 - \zeta = \tilde{\xi} \cos(\sigma t - \tilde{\delta}) \quad (20)$$

with the standard deviation

$$\text{rms}(\tilde{\zeta}) = \frac{1}{2} \sqrt{2\tilde{\xi}}, \quad (21)$$

where

$$\tilde{\xi}^2 = \xi_0^2 - 2\xi_0\xi \cos(\delta_0 - \delta) + \xi^2 \quad (22)$$

and

$$\tan \tilde{\delta} = \frac{\xi_0 \sin \delta_0 - \xi \sin \delta}{\xi_0 \cos \delta_0 - \xi \cos \delta}. \quad (23)$$

Some maximum errors are

$$\tilde{\zeta}_M = \tilde{\xi}_M = \xi_0 + \xi \text{ for } \delta_0 - \delta = 180^\circ, \quad (24)$$

$$\tilde{\zeta}_M = \tilde{\xi}_M = \xi_0 - \xi \text{ for } \delta_0 - \delta = 0^\circ, \quad (25)$$

$$\tilde{\zeta}_M = \tilde{\xi}_M = 2\xi \sin \frac{1}{2}(\delta_0 - \delta) \text{ for } \xi = \xi_0, \quad (26)$$

and

$$\tilde{\zeta}_M = \tilde{\xi}_M = \xi \text{ for } \xi = \xi_0 \text{ and } \delta_0 - \delta = 60^\circ. \quad (27)$$

Equation 27 expresses the important fact that a  $60^\circ$  phase error results in an amplitude error equal to the tidal amplitude and, hence, renders the computed tidal prediction completely useless. Of course, in regions of sufficiently small amplitudes, any phase error is acceptable.

Tables 4A and 4B depict the tidal amplitudes and phases, respectively, of the northwestern Atlantic Ocean including the eastern Caribbean Sea. As can be verified by earlier tide models, this

entire area was very difficult to model, because its rough bottom topography has a strong effect on the tidal currents that sweep over or across various barriers with rapidly changing water levels. There is the broad and shallow continental shelf along the whole North American shoreline, with Cape Hatteras, Long Island, Cape Cod, Nova Scotia, and Newfoundland all protruding into the ocean basin. Furthermore, there are the Grand Banks, the Bahama Banks, and the long and narrow Caribbean Ridge. Obviously, all of the corresponding local tidal features could not be realistically captured by the tide model without a proper representation of the bathymetry (section, "Hydrodynamically Defined Ocean Bathymetry") and without the hydrodynamical interpolation (preceding section) of the locally collected tidal observations.

Now, if one scans the tidal amplitudes and phases (Tables 4A and 4B) from the north to the south, one gathers the impression that the whole computed ocean tide is completely locked into the array of empirical (underlined) tidal data everywhere along the continental coast and along the many aligned islands separating the Atlantic Ocean from the Gulf of Mexico and the Caribbean Sea. It is particularly impressive to see the observed tide data at the offshore islands (Sable—SI, Barbados—BB, and even as far as Bermuda—BI) and at the included nearshore (subbrackets), deep-sea stations all realistically well-accepted by the computed surrounding tide. Moreover, one finds the excluded offshore deep-sea measurements (locations marked by wavy underlines) in the Atlantic and Caribbean Sea fully verified by the independent tide model.

As can be seen in the special listing of Table 3, the measured and computed amplitudes and phases at the Atlantic stations agree within 2 cm and 6°, respectively. The remaining discrepancy is probably within the experimental error due to short observation times and the use of the distant reference station Bermuda (Zettler *et al.*, 1975), which exhibits even larger gaps between the various tidal observations listed in Table 2.

Attention may be drawn to the existence of considerable slopes between the empirical boundary data and the computed ocean-tide

values in the high-amplitude ranges from Nova Scotia to Cape Cod and from Cape Hatteras to Florida's coast. Yet, these rapid tidal variations can be considered as realistic because throughout the same sections the empirical data, among themselves, display exactly the same roughness. This only substantiates clearly the fundamental difference between polynomial and hydrodynamical interpolation techniques pointed out above.

In the complete report (Schwiderski, 1979c I), the same tidal roughness will be recognized in several similar coastal places around the world. From this typical phenomenon, one can draw the fortunate conclusion that, while some empirical data may be lacking high accuracy (see Table 1 and the British Admiralty Tide Tables, 1977 I), the computed adjacent ocean tide may retain its high quality.

In order to gain a deeper insight into the detailed tidal phenomena from the enclosed table charts (e.g., Tables 4A and 4B), it is helpful to recall the physical meaning of the tabulated tidal constants. The local tidal amplitude,  $\xi$ , is defined as half the tidal "range," which measures the total variation of the water level from high to low. Lines of constant amplitudes are called "corange lines." The local phase,  $\delta$ , specifies the tidal cresting time (in degrees) after the moon's (or sun's) passage over the Greenwich meridian. For the present  $M_2$ -tide one has the following time conversions:

$$\begin{aligned} 360^\circ &= 12.421 \text{ hr (period),} \\ 30^\circ &= 1.035 \text{ hr,} \\ 1^\circ &= 2.070 \text{ min.} \end{aligned} \tag{28}$$

Lines of constant phases (simultaneous cresting times) are called "cotidal lines." In particular, at the  $0^\circ = 360^\circ$  cotidal lines, which are conspicuously visible in the phase charts (Tables 4B to 7B), the tide crests simultaneously with the moon's passage over the Greenwich meridian. The tidal crest advances with time normal to the cotidal lines toward larger phases. A point of zero amplitude ( $\xi = 0$ ) around which the tidal crest rotates from  $0^\circ$  to  $360^\circ$  is called an "amphidromic point"; it is marked in the tables by a circled star  $\odot$ .

**M** = Longitude east (°).  
**N** = Colatitude (°).  
**☆** = Amphidromic point.  
**—** = Subbars mark empirical input data.  
**[ ]** = Subbrackets mark input nearshore deep-sea measurements.  
**~** = Wavy underlines mark offshore deep-sea tide gauge stations with excluded measurements listed in Table 3a, b.

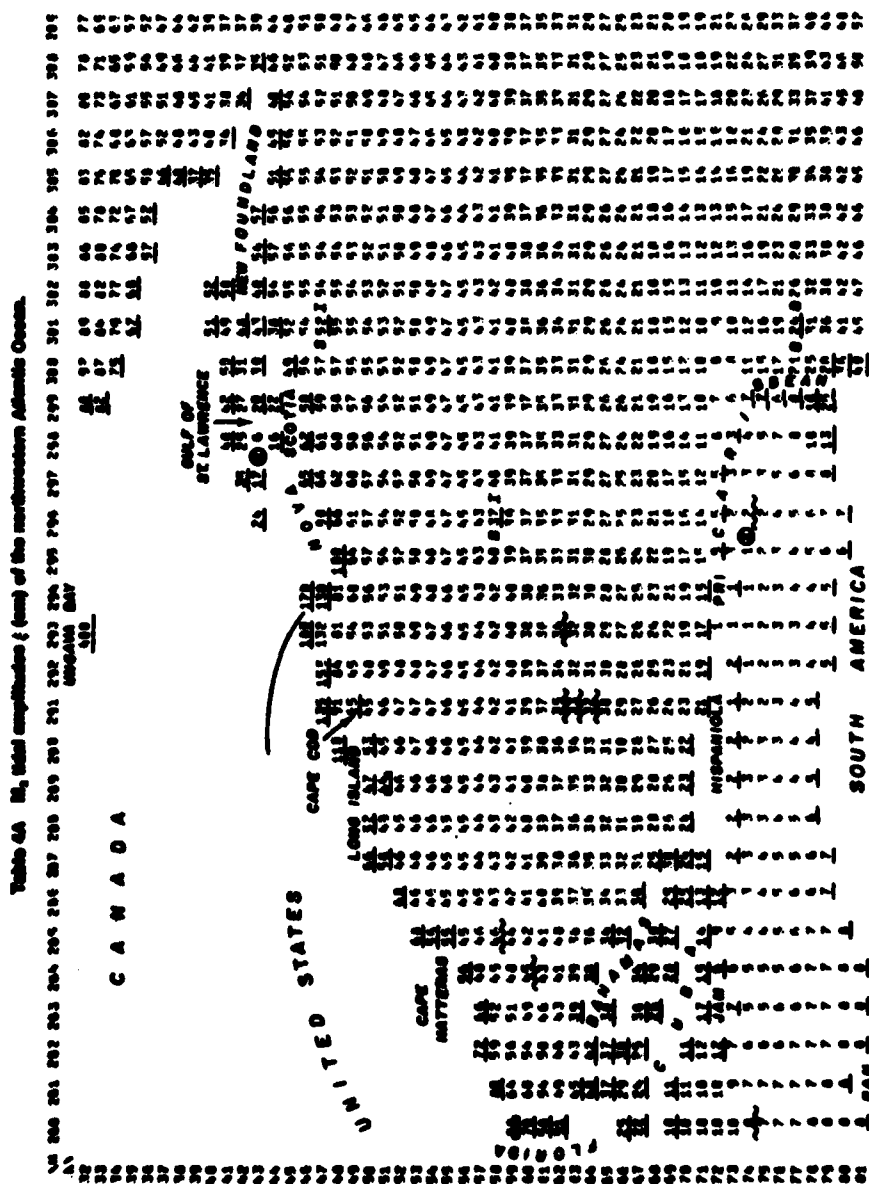


Table 45 Males, third phases 3 (°) of the northwestern Atlantic Ocean.

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**Table 5A**  $M_2$  tidal amplitudes  $\xi$  (cm) of the northeastern Pacific Ocean.

[illegible]



Table 8B. In, tidal phases 8 (°) of the northeastern Pacific Ocean.

210	217	224	231	238	245	252	259	266	273	280	287	294	301	308	315	322	329	336	343	350	357	364	371	378	385	392	399	406	413	420	427	434	441	448	455	462	469	476	483	490	497	504	511	518	525	532	539	546	553	560	567	574	581	588	595	602	609	616	623	630	637	644	651	658	665	672	679	686	693	700	707	714	721	728	735	742	749	756	763	770	777	784	791	798	805	812	819	826	833	840	847	854	861	868	875	882	889	896	903	910	917	924	931	938	945	952	959	966	973	980	987	994	1001	1008	1015	1022	1029	1036	1043	1050	1057	1064	1071	1078	1085	1092	1099	1106	1113	1120	1127	1134	1141	1148	1155	1162	1169	1176	1183	1190	1197	1204	1211	1218	1225	1232	1239	1246	1253	1260	1267	1274	1281	1288	1295	1302	1309	1316	1323	1330	1337	1344	1351	1358	1365	1372	1379	1386	1393	1400	1407	1414	1421	1428	1435	1442	1449	1456	1463	1470	1477	1484	1491	1498	1505	1512	1519	1526	1533	1540	1547	1554	1561	1568	1575	1582	1589	1596	1603	1610	1617	1624	1631	1638	1645	1652	1659	1666	1673	1680	1687	1694	1701	1708	1715	1722	1729	1736	1743	1750	1757	1764	1771	1778	1785	1792	1799	1806	1813	1820	1827	1834	1841	1848	1855	1862	1869	1876	1883	1890	1897	1904	1911	1918	1925	1932	1939	1946	1953	1960	1967	1974	1981	1988	1995	2002	2009	2016	2023	2030	2037	2044	2051	2058	2065	2072	2079	2086	2093	2100	2107	2114	2121	2128	2135	2142	2149	2156	2163	2170	2177	2184	2191	2198	2205	2212	2219	2226	2233	2240	2247	2254	2261	2268	2275	2282	2289	2296	2303	2310	2317	2324	2331	2338	2345	2352	2359	2366	2373	2380	2387	2394	2401	2408	2415	2422	2429	2436	2443	2450	2457	2464	2471	2478	2485	2492	2499	2506	2513	2520	2527	2534	2541	2548	2555	2562	2569	2576	2583	2590	2597	2604	2611	2618	2625	2632	2639	2646	2653	2660	2667	2674	2681	2688	2695	2702	2709	2716	2723	2730	2737	2744	2751	2758	2765	2772	2779	2786	2793	2800	2807	2814	2821	2828	2835	2842	2849	2856	2863	2870	2877	2884	2891	2898	2905	2912	2919	2926	2933	2940	2947	2954	2961	2968	2975	2982	2989	2996	3003	3010	3017	3024	3031	3038	3045	3052	3059	3066	3073	3080	3087	3094	3101	3108	3115	3122	3129	3136	3143	3150	3157	3164	3171	3178	3185	3192	3199	3206	3213	3220	3227	3234	3241	3248	3255	3262	3269	3276	3283	3290	3297	3304	3311	3318	3325	3332	3339	3346	3353	3360	3367	3374	3381	3388	3395	3402	3409	3416	3423	3430	3437	3444	3451	3458	3465	3472	3479	3486	3493	3500	3507	3514	3521	3528	3535	3542	3549	3556	3563	3570	3577	3584	3591	3598	3605	3612	3619	3626	3633	3640	3647	3654	3661	3668	3675	3682	3689	3696	3703	3710	3717	3724	3731	3738	3745	3752	3759	3766	3773	3780	3787	3794	3801	3808	3815	3822	3829	3836	3843	3850	3857	3864	3871	3878	3885	3892	3899	3906	3913	3920	3927	3934	3941	3948	3955	3962	3969	3976	3983	3990	3997	4004	4011	4018	4025	4032	4039	4046	4053	4060	4067	4074	4081	4088	4095	4102	4109	4116	4123	4130	4137	4144	4151	4158	4165	4172	4179	4186	4193	4200	4207	4214	4221	4228	4235	4242	4249	4256	4263	4270	4277	4284	4291	4298	4305	4312	4319	4326	4333	4340	4347	4354	4361	4368	4375	4382	4389	4396	4403	4410	4417	4424	4431	4438	4445	4452	4459	4466	4473	4480	4487	4494	4501	4508	4515	4522	4529	4536	4543	4550	4557	4564	4571	4578	4585	4592	4599	4606	4613	4620	4627	4634	4641	4648	4655	4662	4669	4676	4683	4690	4697	4704	4711	4718	4725	4732	4739	4746	4753	4760	4767	4774	4781	4788	4795	4802	4809	4816	4823	4830	4837	4844	4851	4858	4865	4872	4879	4886	4893	4900	4907	4914	4921	4928	4935	4942	4949	4956	4963	4970	4977	4984	4991	4998	5005	5012	5019	5026	5033	5040	5047	5054	5061	5068	5075	5082	5089	5096	5103	5110	5117	5124	5131	5138	5145	5152	5159	5166	5173	5180	5187	5194	5201	5208	5215	5222	5229	5236	5243	5250	5257	5264	5271	5278	5285	5292	5299	5306	5313	5320	5327	5334	5341	5348	5355	5362	5369	5376	5383	5390	5397	5404	5411	5418	5425	5432	5439	5446	5453	5460	5467	5474	5481	5488	5495	5502	5509	5516	5523	5530	5537	5544	5551	5558	5565	5572	5579	5586	5593	5600	5607	5614	5621	5628	5635	5642	5649	5656	5663	5670	5677	5684	5691	5698	5705	5712	5719	5726	5733	5740	5747	5754	5761	5768	5775	5782	5789	5796	5803	5810	5817	5824	5831	5838	5845	5852	5859	5866	5873	5880	5887	5894	5901	5908	5915	5922	5929	5936	5943	5950	5957	5964	5971	5978	5985	5992	5999	6006	6013	6020	6027	6034	6041	6048	6055	6062	6069	6076	6083	6090	6097	6104	6111	6118	6125	6132	6139	6146	6153	6160	6167	6174	6181	6188	6195	6202	6209	6216	6223	6230	6237	6244	6251	6258	6265	6272	6279	6286	6293	6300	6307	6314	6321	6328	6335	6342	6349	6356	6363	6370	6377	6384	6391	6398	6405	6412	6419	6426	6433	6440	6447	6454	6461	6468	6475	6482	6489	6496	6503	6510	6517	6524	6531	6538	6545	6552	6559	6566	6573	6580	6587	6594	6601	6608	6615	6622	6629	6636	6643	6650	6657	6664	6671	6678	6685	6692	6699	6706	6713	6720	6727	6734	6741	6748	6755	6762	6769	6776	6783	6790	6797	6804	6811	6818	6825	6832	6839	6846	6853	6860	6867	6874	6881	6888	6895	6902	6909	6916	6923	6930	6937	6944	6951	6958	6965	6972	6979	6986	6993	7000	7007	7014	7021	7028	7035	7042	7049	7056	7063	7070	7077	7084	7091	7098	7105	7112	7119	7126	7133	7140	7147	7154	7161	7168	7175	7182	7189	7196	7203	7210	7217	7224	7231	7238	7245	7252	7259	7266	7273	7280	7287	7294	7301	7308	7315	7322	7329	7336	7343	7350	7357	7364	7371	7378	7385	7392	7399	7406	7413	7420	7427	7434	7441	7448	7455	7462	7469	7476	7483	7490	7497	7504	7511	7518	7525	7532	7539	7546	7553	7560	7567	7574	7581	7588	7595	7602	7609	7616	7623	7630	7637	7644	7651	7658	7665	7672	7679	7686	7693	7700	7707	7714	7721	7728	7735	7742	7749	7756	7763	7770	7777	7784	7791	7798	7805	7812	7819	7826	7833	7840	7847	7854	7861	7868	7875	7882	7889	7896	7903	7910	7917	7924	7931	7938	7945	7952	7959	7966	7973	7980	7987	7994	8001	8008	8015	8022	8029	8036	8043	8050	8057	8064	8071	8078	8085	8092	8099	8106	8113	8120	8127	8134	8141	8148	8155	8162	8169	8176	8183	8190	8197	8204	8211	8218	8225	8232	8239	8246	8253	8260	8267	8274	8281	8288	8295	8302	8309	8316	8323	8330	8337	8344	8351	8358	8365	8372	8379	8386	8393	8400	8407	8414	8421	8428	8435	8442	8449	8456	8463	8470	8477	8484	8491	8498	8505	8512	8519	8526	8533	8540	8547	8554	8561	8568	8575	8582	8589	8596	8603	8610	8617	8624	8631	8638	8645	8652	8659	8666	8673	8680	8687	8694	8701	8708	8715	8722	8729	8736	8743	8750	8757	8764	8771	8778	8785	8792	8799	8806	8813	8820	8827	8834	8841	8848	8855	8862	8869	8876	8883	8890	8897	8904	8911	8918	8925	8932	8939	8946	8953	8960	8967	8974	8981	8988	8995	9002	9009	9016	9023	9030	9037	9044	9051	9058	9065	9072	9079	9086	9093	9100	9107	9114	9121	9128	9135	9142	9149	9156	9163	9170	9177	9184	9191	9198	9205	9212	9219	9226	9233	9240	924
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Table 7A.  $M_1$  tidal amplitudes  $\xi$  (cm) of the central Pacific Ocean.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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In the area of Tables 4A and 4B, a major amphidromic point is visible in the Caribbean Sea southeast of the island of Puerto Rico (PRI) near the marked deep-sea gauge station. The loosely connected Caribbean and Atlantic tides rotate counterclockwise around this point with the  $0^\circ = 360^\circ$  cotidal line running northeastward. As a result of this rotation, the whole Caribbean Sea appears to be trapped and unable to develop any significant  $M_2$ -tide. In agreement with the observations, the  $M_2$  tidal crest sweeps across the Caribbean Sea essentially from north to south with very little variation in water level.

If one follows the tidal crest around the amphidromic point from the Atlantic Ocean to the Caribbean Sea and back to the Atlantic, one recognizes a major tidal distortion caused by ocean ridges, which has long been discovered by practical tidalists (see, e.g., Harris, 1904 I; Bogdanov, 1961 I; Defant, 1961 I; and Luther and Wunsch, 1974 I). As the tide crosses the ridge between the islands, it suffers a distinct amplitude jump and a significant phase shift. For example, north of Puerto Rico (PRI) and Hispaniola and in the southeast around Barbados (BB), the computed and empirical Atlantic tide data display a higher water level and an earlier or, respectively, a delayed cresting time than the adjacent tide data on the Caribbean side. In particular, in full agreement with the observations, the tidal retardation time can easily exceed  $30^\circ$  ( $\sim 1$  hour). The distortion seems to depend on the angle with which the tidal crest spills over the ridge. Maximum distortion appears to be associated with a normal crossing. It may be pointed out that the realistic resolution of tidal distortions by ocean ridges (see below) constitutes probably the most significant improvement of the new model over all earlier hydrodynamical models.


The Atlantic portion of the Caribbean-Atlantic amphidromic rotation is opposed by a southward advancing tide from about Newfoundland in the north and by an eastward progressing tide from about Cape Cod to Cape Hatteras in the west. As a result of this interaction of three opposing tidal waves, the middle latitudes (around  $n = 60^\circ$ ) of the Atlantic display very small variations in tidal amplitudes and phases. In the high-amplitude sections be-

tween Nova Scotia and Cape Cod and between Cape Hatteras and Florida's coast, the Caribbean-Atlantic rotation wave seems to be less affected by the opposing tidal waves and progresses frontally against the corresponding shallow coastal corners.

Since the tide-generating  $M_2$ -potential is a single progressing wave from east to west, the ocean responds with amphidromic tidal waves that cannot reverse their directions. Thus, at shore points tidal waves are either incoming or outgoing without reversals. In the first case tidal crests always move from sea to shore. In the second case tides always swell to their crests at the shore first and then move out to sea. The incoming tide between Nova Scotia and Cape Cod seems to produce high and rough waters. The outgoing tide between Cape Cod and Cape Hatteras is distinctly lower.

Although the computed tide in the Gulf of St. Lawrence displays the well-known amphidromic point (Defant, 1961 I), the grid system is much too crude to attach a high accuracy to the tidal constants in this border sea. For the same reason, the tidal data listed between Florida, Cuba, and the Bahamas are naturally less accurate than those in the open oceans.

Tables 5A and 5B illustrate the smoothness with which the computed tide of the northeastern Pacific Ocean attaches itself to the empirical tide data along the North American west coast. The tidal constants observed at the islands of Guadalupe (GI) and Farallon (FI), at the Cobb Seamount (CS), and at the included nearshore deep-sea stations fit realistically well into the computed surrounding tide. The amplitudes and phases of the excluded offshore deep-sea measurements in the Pacific agree within 2 cm and 6°, respectively, with the computed data (Table 3), which is just the same accuracy as in the Atlantic.

Perhaps the most prominent feature of this area is the amphidromic point , around which the  $M_2$ -tide rotates counterclockwise. This amphidromic system was predicted by Munk *et al.* (1970) and Irish *et al.* (1971) in almost identical geographical position. Earlier hydrodynamical tide models failed to resolve this system on proper location, although several models matched the empirical data along the coast quite well. Since the northeastern

Pacific falls short in major bottom and coastal irregularities when compared to the northwestern Atlantic, the indicated rapid loss of quality in westerly direction seemed disappointing. Yet, as will be demonstrated below, this shortcoming could have been concluded from the obvious failure of those models to reasonably reproduce the tide over most of the north and central Pacific Ocean.

As was mentioned before, the author's preliminary tide model (Schwiderski, 1976 I) used a bathymetry that failed to represent the hydrodynamical barrier effects of the Marianas, Nampo, Kuril, Aleutian, and Hawaiian ridges, as well as of other seamount chains. Consequently, the  $M_2$ -tide of almost the whole central, western, and northern Pacific area was modeled as a single huge amphidromic system, as pictured by the similar maps of other numerical tidalists such as Zahel (1971 I) and Estes (1975 I, 1977 I). The clockwise-rotating Pacific tide was free to sweep undisturbed into the Philippine, Okhotsk, and Bering seas. By the time the computed tidal crest reached the Aleutian Islands, it was just about  $180^\circ$  out of phase. When the original bathymetry was replaced by hydrodynamically defined depth data (section, "Hydrodynamically Defined Ocean Bathymetry"), the entire Pacific Ocean resembled a whirlpool after some continued computations over several quarter periods. The amphidromic system weakened, and its center slipped slowly southward, but drastically improved phases appeared gradually along the Aleutian Ridge, confirming the anticipated effect of ocean ridges.

The complete turnaround of the Pacific  $M_2$  tide near the Aleutian Islands was speeded up when the empirical tidal constants were introduced into the model. In fact, a repeat of the same computations settled the Pacific Ocean tide into its final position in a rather dramatic fashion. Striking improvements were registered over the whole Pacific and, of course, also over the Atlantic and Indian oceans.

As is depicted in Tables 6A and 6B for the north-central Pacific, the amphidromic system is replaced by a low-amplitude tide. It appears to be locked in between the Aleutian and Hawaiian ridges in the north and south and also between the Emperor Seamount



chain in the west and the high-amplitude tide in the east, which progresses in a westerly direction from the west coast of North America (Tables 5A and 5B). The amplitude topography of this area resembles the low-amplitude tide in the Caribbean Sea (Table 4A). When the westward-advancing tidal wave enters the region between the Aleutian and Hawaiian ridges, it suffers a remarkable, almost symmetric retardation at both ridges. In fact, as the visible ( $0^\circ = 360^\circ$ ) cotidal line in Table 6B reveals, the crest front of the tidal wave assumes the shape of an almost symmetric wedge. If one traces the  $0^\circ$  phase line westward beginning at both ridges, one can infer a definite idea about the realistic reproduction of the tide in this region. At both ends, the  $0^\circ$  phase is in full agreement with the empirical data. As the observed phases grow westward along both ridges, so grow proportionally the distances of the  $0^\circ$  phase line from the ridges.

The new computed  $M_2$ -tide model no longer indicates any symptoms of the original phase problems at the Aleutian and Hawaiian ridges. The computed amplitudes and phases approach the empirical tidal constants from both sides of the ridges as smoothly as could be desired. As the tidal wave spills over both ridges in north-westward or southwestward directions, respectively, it suffers a tidal distortion similar to that found before at the Caribbean Ridge. Amplitude jumps and major phase shifts are again in complete agreement with observations (see the remarks of Luther and Wunsch, 1974 I). It is particularly gratifying to find the phase shift well developed along the whole length of the Hawaiian Ridge from the island of Hawaii to Midway, even though only few stations of data were used at both ends. Also, it may be noticed that the observed tidal constants at the distant and isolated island stations of Pribilof (PF), Midway (MW), and Johnston (JI) are all realistically well integrated by the surrounding computed tide.

Ironically, the old and new  $M_2$ -tide maps constructed by Bogdanov (1961 I) and Luther and Wunsch (1974 I) by pure intuition and simple rules of thumb from empirical data came closest to the present charts. Indeed, their maps display no amphidromic system in the north-central Pacific. As is verified in Schwiderski

(1979c I), the computed amphidromic points between the Cook and Society islands and near the southern edge of the Solomon Islands are both in almost identical positions with those charted by the same authors. Nevertheless, their detailed distribution of amplitudes and phases is still significantly different from the present one.

Perhaps the most spectacular display of the high quality of both the computed and the observed tidal data is brought out by Tables 7A and 7B depicting the high-amplitude tide of the central Pacific. Indeed, unlike any other open ocean area, the tabulated region is dotted with numerous tide-gauge stations at island groups and at scattered isolated islands. In addition to the fully listed island chains, there are the isolated islands: Johnston (JI), Wake (WI), Kudaie (KI), Ocean (OI), Funafuti (FI), Wallis (WI), Niue (NI), and Norfolk (NF). The corresponding observed tidal constants listed in nongeographical arrangement appeared incoherent and, hence, uncorrelated, giving rise to doubt their true value. Yet, the computed tidal wave sweeps across the whole area in a south-westerly direction with little variation of its high amplitude. As the wave crest passes through the many checkpoints with correct height and in right time, it integrates and correlates without a single exception all the empirical data into one coherent unity.

### Conclusions

The quality evaluation of the constructed  $M_2$  ocean tide model described in Parts I and II of this paper leads to the conclusion that it is now possible to compute detailed and accurate global ocean tides which fulfill the application requirements of contemporary researchers. In fact, it is estimated that the computed  $M_2$ -tide charts permit an  $M_2$ -tide prediction anywhere in the open oceans with an accuracy of better than 5 cm. This accuracy leaves ample room for superposable errors due to the additional smaller tidal constituents listed in Table 1 of Part I, which are presently under construction with equivalent relative accuracy. When all those partial tides become available, the total tide-prediction error is expected to fall well below the 10-cm limit needed in many applications.

Naturally, the achieved high accuracy of the  $M_2$ -tide in the open

oceans drops somewhat near continental or island stations where empirical data are missing or are less accurate themselves (see the introduction to the British Admiralty Tide Tables, 1977 I). This is particularly true near Antarctica and in the Arctic Ocean, where reliable measurements of ocean tides and depths are sparse. Also, less accurate predictions must be anticipated in small border seas, bays, estuaries, and channels where the  $1^\circ$  by  $1^\circ$  grid system precludes a sufficient resolution. To improve the present tide model in those areas, significantly improved observations will be needed along with a locally refined network and corresponding bathymetric data.

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